

Raw test data was processed to calculate dU_{cyc}/dN , dU_{tot}/dN , G_{max} and $(\Delta\sqrt{G})^2$. The steps taken in data processing are given as under. Following steps are carried out using fatigue test data at 40°C and R=0.61.

- Crack length calculated from the CCD camera images is plotted against number of cycles N .

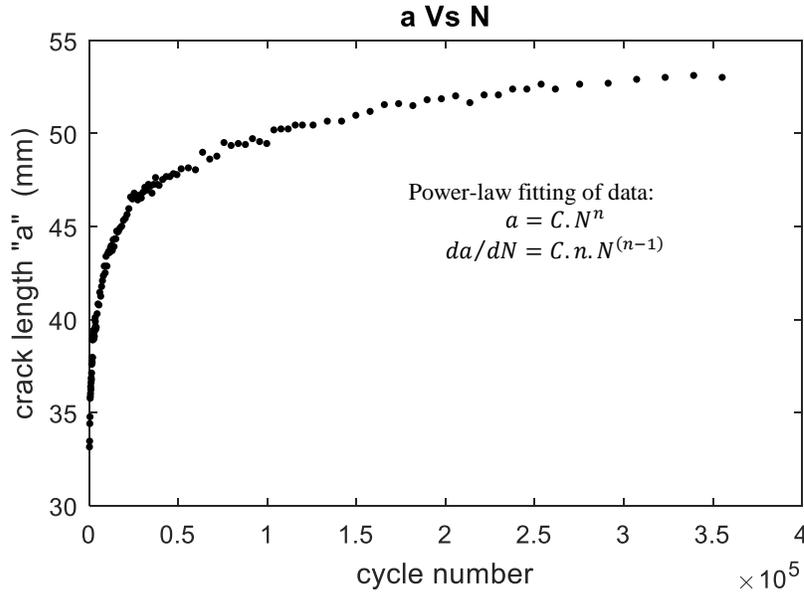


Figure 1 "a Vs N" plot with curve fitting

- Derivative of the power-law fit equation shown in Figure 1 gives the slope of the curve which is the rate of growth of fatigue crack i.e. da/dN .
- Rate of formation of crack surface dA/dN is obtained by multiplying da/dN with width of the DCB specimen b .
- Maximum and minimum strain energy release rate G_{max} and G_{min} was calculated using the compliance calibration method given in ASTM 5528-01 (2007).

$$G = \frac{nPd}{2ba} \quad (1)$$

Where P is the applied load, d is the displacement, a is the crack length and b is the specimen width. n is the slope of the plot between $\log C$ and $\log a$. n was calculated for every test data. Where C is compliance (displacement/load).

$$C = \frac{d_{max} - d_{min}}{F_{max} - F_{min}} \quad (2)$$

- $(\Delta\sqrt{G})^2$ or simply $(\Delta\sqrt{G})$ was calculated as suggested by (Rans, et al., 2011)

$$(\Delta\sqrt{G})^2 = (\sqrt{G_{max}} - \sqrt{G_{min}})^2 \quad (3)$$

- In the fatigue loading, cyclic energy U_{cyc} and monotonic energy U_{mono} can be defined from the load-displacement diagram Figure 2.

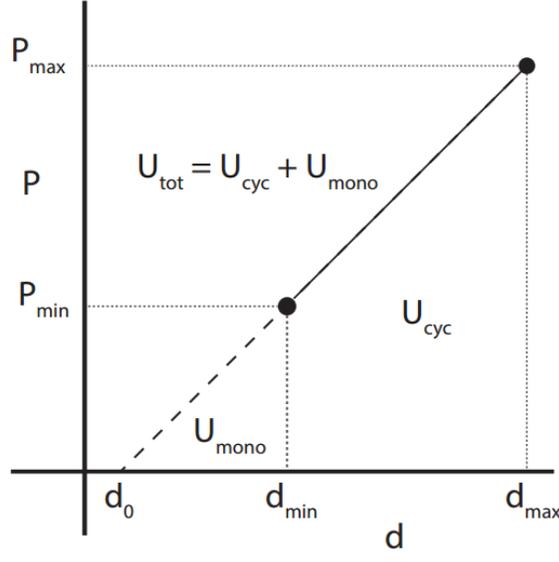


Figure 2 Load-Displacement diagram with the definition of U_{mono} and U_{cyc} (Pascoe, et al., 2016)

Where U_{cyc} is the energy that is supplied to the DCB specimen during each loading half cycle. U_{mono} is the energy that is still in the specimen after the unloading half cycle. Furthermore, it was observed that in most of the cases the curve plotted between $P - d$ does not pass through the origin which means that there is still some value of displacement (d_0) when force F is zero as shown in Figure 2.

From Figure 2, U_{cyc} , U_{mono} and U_{tot} can be defined as under.

$$U_{cyc} = \frac{1}{2} P_{max} (d_{max} - d_0) - \frac{1}{2} P_{min} (d_{min} - d_0) \quad (4)$$

$$U_{tot} = \frac{1}{2} P_{max} (d_{max} - d_0) \quad (5)$$

Where U_{tot} is the sum of U_{mono} and U_{cyc} . Cyclic and total energy are calculated from the raw test data and plotted against number of cycles N . U_{cyc} and U_{tot} are plotted against number of cycles N .

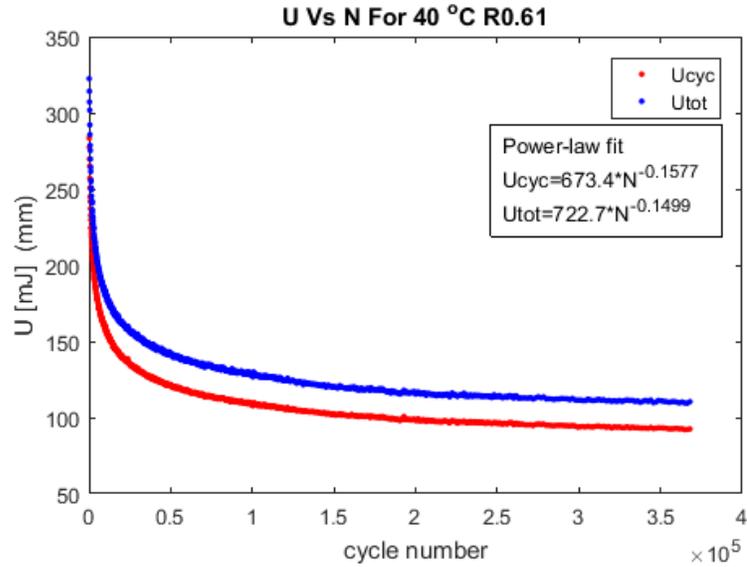


Figure 3 U_{cyc} and U_{tot} plotted against N for specimen 40 R0.61

First derivative of the power law curve fitting equations as mentioned in Figure 3 gives $-dU_{cyc}/dN$ and $-dU_{tot}/dN$. Same steps were carried out for the data of all tests.

Name of the test data gives the information of the test temperature and the applied R-ratio, For example “40 R0.61” means the specimen that was tested at 40°C and at R-ratio 0.61. In some cases, when same test was repeated, letter ‘R’ has been added at the end of the data/test name for example “-55 R0.036 R” means this is test was repeated at -55°C and R= 0.036.

Width of each specimen was measure using a calliper. Table-1 shows the width of each specimen.

Table 1 Specimen width

| Test Name | Specimen width ‘b’ (mm) | Test Name | Specimen width ‘b’ (mm) |
|--------------|-------------------------|-------------|-------------------------|
| -55 R0.036 | 24.99 | RT R0.61 | 25.01 |
| -55 R0.29 | 24.98 | 40 R0.036 | 24.98 |
| -55 R0.61 | 24.99 | 40 R0.29 | 24.97 |
| -55 R0.61 R | 24.98 | 40 R0.61 | 24.97 |
| -20 R0.036 | 25.01 | 60 R0.036 | 25.01 |
| -20 R0.036 R | 24.98 | 60 R0.036 R | 25.01 |
| -20 R0.29 | 24.95 | 60 R0.29 | 25.02 |
| -20 R0.61 | 24.99 | 60 R0.61 | 24.98 |
| -20 R0.61 R | 25.02 | 80 R0.036 | 25 |
| ZeroR0.036 | 25.02 | 80 R0.29 | 25.01 |
| ZeroR0.29 | 25.02 | 80 R0.61 | 25.01 |
| ZeroR0.61 | 25.02 | 80 R0.61R | 25.01 |
| RT R0.036 | 25.01 | | |
| RT R0.29 | 24.98 | | |

References

Pascoe, J., Alderliesten, R. & Benedictus, R., 2016. Characterising resistance to fatigue crack growth in adhesive bonds by measuring release of strain energy. *Structural Integrity Procedia*. (Submitted for Publication).

Rans, C., Alderliesten, . R. & Benedictus, R., 2011. Misinterpreting the results: how similitude can improve our understanding of fatigue delamination growth. *Compos Sci Technol*, Volume 71, pp. 230-238.